

**Satellite Communication and Positioning Systems – Prof. L. Luini,  
July 9<sup>th</sup>, 2024**

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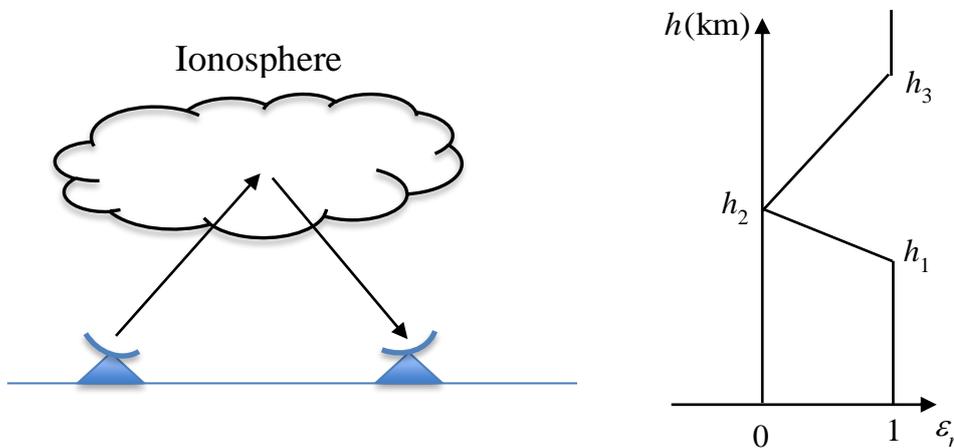
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**Problem 1**

Making reference to the figure below, a communication system exploits the ionosphere during nighttime: it operates at  $f = 3.6$  MHz and works with elevation angle  $\theta = 30^\circ$ . The trend of  $\epsilon_r$  in the ionosphere is depicted in the figure below on the right side ( $h_1 = 100$  km,  $h_2 = 200$  km and  $h_3 = 400$  km). Calculate the distance between the stations to enable the communication.

Assumptions: no tropospheric effects; flat Earth; virtual reflection height  $h_V = 1.2 h_R$  ( $h_R$  being the real reflection height).



**Solution**

The peak electron content value can be obtained from the following expression:

$$\sqrt{1 - \left(\frac{9\sqrt{N_{\max}}}{f}\right)^2} = \sqrt{\min(\epsilon_r)}$$

Setting  $\epsilon_r = 0$  as from the graph on the right, inverting the expression  $\rightarrow N_{\max} = 16 \times 10^{10} \text{ e/m}^3$ .  $N_{\max}$  obviously corresponds to the lowest value of  $\epsilon_r$ , but, as the link is not zenithal, the reflection will occur somewhere below  $h_2$ . In fact, the reflection point depends on  $N$  through the following expression:

$$\sqrt{1 - \left(\frac{9\sqrt{N}}{f}\right)^2} = \cos(\theta)$$

Inverting the expression  $\rightarrow N = 4 \times 10^{10} \text{ e/m}^3$ . Given the trend of  $\varepsilon_r \rightarrow N(h_1) = 0 \text{ e/m}^3$  and  $N(h_2) = N_{\max} = 16 \times 10^{10} \text{ e/m}^3$ . Therefore, the value of  $h$  (up to  $h_2$ ) as a function of  $N$  is:

$$h = \frac{h_2 - h_1}{N_{\max}} N + h_1$$

Using  $N = 4 \times 10^{10} \text{ e/m}^3 \rightarrow h = 125 \text{ km}$ . The distance between the station is:

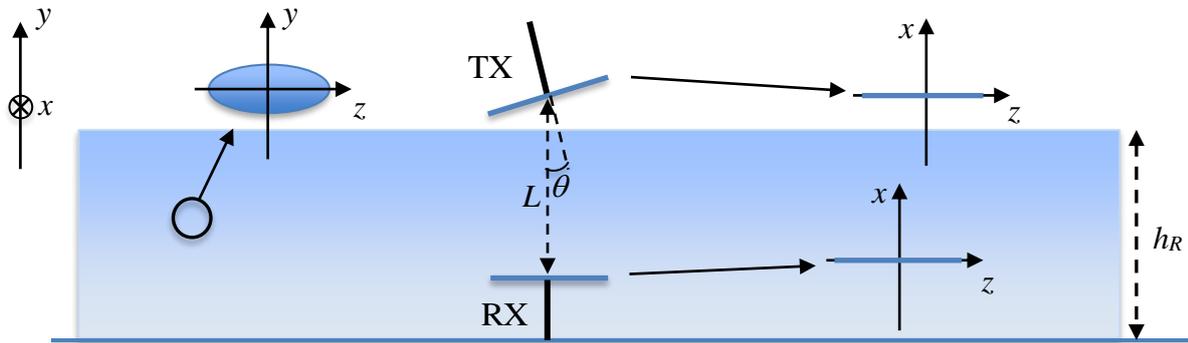
$$D = 2 \frac{h_V}{\tan(\theta)} = 2 \frac{1.2h_R}{\tan(\theta)} \approx 520 \text{ km}$$

## Problem 2

An Earth-space link, with path length  $L = 500$  km and operating at  $f = 900$  MHz, crosses a rain layer with thickness  $h_R = 2$  km (raindrops all aligned as shown in the sketch below). Both the transmitter (TX) and the receiver (RX) use linear horizontal antennas, but the TX antenna is tilted by  $\theta = 30^\circ$  as shown in the sketch below, due to issues in the satellite attitude control. For this link:

- 1) Determine the polarization of the wave in front of the receiver RX (specify: LH or RH for a circular/elliptical, tilt angle for a linear).
- 2) Calculate the power received by RX.

Assume: transmit power  $P_T = 200$  W; gain of the antennas  $G = 8$  dB; radiation pattern of the antennas  $f = [\cos(\theta)]^2$ .



## Solution

1) As the operational frequency is much lower than 10 GHz, the wave is unaffected by the presence of rain along the path, both in terms of attenuation and delay. This means that no depolarization effects can take place.

2) Given the operational frequency, tropospheric and ionospheric attenuation can be neglected. Thus, the power received by RX is simply:

$$P_R = P_T G_T f_T \left( \frac{\lambda}{4\pi L} \right)^2 f_R G_R \approx 16.8 \text{ pW}$$

where,  $f_T = 1$ ,  $f_R = [\cos(\theta)]^2 = 0.75$ ,  $G_T = G_R = 6.3$ ,  $\lambda = 0.334$  m.

### **Problem 3**

Consider a GNSS receiver onboard a geosynchronous (GSO) satellite:

- 1) Is the GSO satellite positioning possible? Justify your answer.
- 2) If the answer to the previous point is yes, discuss the main limitation(s) in the GSO satellite positioning accuracy.

### **Solution**

1) It is in principle possible: the GNSS signals can reach the GEO satellite through the side lobes of the GNSS satellite antenna.

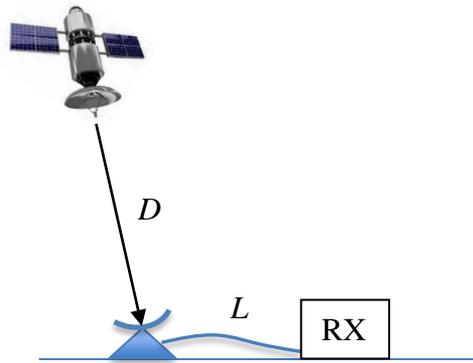
2) Though possible, the positioning accuracy will be strongly impaired by: low SNR (large distance); high Dilution of Precision (poor satellites geometry).

#### Problem 4

Consider the downlink from a GEO satellite to a ground station consisting of a VSAT (Very Small Aperture Terminal), operating at  $f = 25$  GHz. The VSAT consists of a typical reflector antenna with a feed and a transmission line (specific attenuation  $\alpha_{TL} = 1$  dB/m) guiding the signal from the feed to the receiver RX. Determine the maximum length  $L$  of the transmission line to guarantee a minimum signal-to-noise ratio (SNR) of 5 dB at the receiver. The link undergoes tropospheric attenuation; the zenithal trend of the specific attenuation  $\alpha$  is given by:

$$\alpha(h) = 5e^{-0.5h} \quad (\alpha \text{ is in dB/km and } h \text{ is the height in km})$$

Estimate the maximum data rate  $R$  achievable with this link. Finally, will  $R$  likely increase or decrease if the carrier frequency changes to 22 GHz?



Additional assumptions and data:

- elevation angle  $\theta = 30^\circ$
- power transmitted by the satellite  $P_T = 400$  W
- antennas optimally pointed
- mean radiating temperature  $T_{mr} = 280$  K
- gain of the antennas:  $G_T = 40$  dB,  $G_R = 20$  dB
- distance to the satellite  $D = 37000$  km
- bandwidth of the receiver  $B = 1$  MHz
- internal noise temperature of the receiver  $T_R = 250$  K
- physical temperature of the transmission line  $T_P = 295$  K
- no additional losses in the transmitter and the receiver
- troposphere: horizontally homogeneous

#### Solution

The signal-to-noise ratio (SNR) is given by

$$SNR = \frac{P_T G_T f_T (\lambda/4\pi D)^2 G_R f_R A_S}{k [T_A + T_{TL} + T_R/A_{TL}] B}$$

where  $A_S$  is the slant path attenuation in linear scale,  $T_{TL}$  is the equivalent noise temperature of the transmission line,  $A_{TL}$  is the transmission line attenuation in linear scale,  $f_T = f_R = 1$ ,  $k$  is the Boltzmann's constant ( $1.38 \times 10^{-23}$  J/K) and  $T_A$  is the equivalent antenna noise temperature. The latter is calculated as:

$$T_A = A_S T_C + T_{mr} (1 - A_S)$$

with  $T_C = 2.73$  K. Let us calculate the zenithal tropospheric attenuation as:

$$A_Z = \int_0^{30 \text{ km}} \alpha(h) dh = \int_0^{30 \text{ km}} 5e^{-0.5h} dh \approx \int_0^{\infty} 5e^{-0.5h} dh = \frac{5}{0.5} = 10 \text{ dB}$$

The slant attenuation, in linear scale, is:

$$A_S = 10^{-\frac{A_Z}{10 \sin(\theta)}} = 0.01$$

Numerically  $\rightarrow T_A = 277$  K.

As for the transmission line equivalent noise temperature:

$$T_{TL} = T_P \left( \frac{1}{A_{TL}} - 1 \right)$$

$A_{TL}$  is defined as:

$$A_{TL} = 10^{-\frac{\alpha_{TL} L}{10}}$$

where  $L$  is in m.

Therefore, imposing  $SNR_{\min} = 5 \text{ dB} = 3.16$ :

$$SNR = \frac{P_T G_T (\lambda/4\pi D)^2 G_R A_S}{k \left[ T_A + T_P \left( \frac{1}{A_{TL}} - 1 \right) + T_R / A_{TL} \right] B} = 3.16$$

Inverting the equation above to solve for  $L$  in  $A_{TL}$  (one solution is an acceptable real number, the other one is a complex number)

$$L \approx 12.35 \text{ m}$$

The maximum data rate  $R$  is given the Shannon limit:

$$R = B \log_2(1 + SNR) \approx 2.3 \text{ Mb/s}$$

If the carrier frequency shifts to 22 GHz, the wavelength will slightly increase (so the free space loss will slightly decrease), but there will be a strong increase in the tropospheric attenuation due to water vapor absorption peak. This will cause a decrease in the  $SNR$  and, consequently, in  $R$ .