# Electromagnetics and Signal Processing for Spaceborne Applications - EM part 

September 6 ${ }^{\text {th }}, 2022$


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## Problem 1

A source with voltage $V_{g}=10 \mathrm{~V}$ and internal impedance $Z_{g}=50 \Omega$ is connected to a transmission line with characteristic impedance $Z_{C}=75 \Omega$, which terminates on a load $Z_{L}=50 \Omega$. The frequency is $f=300 \mathrm{MHz}$ and the length of the line is $l=5.25 \mathrm{~m}$.

1) Calculate the power absorbed by $Z_{L}$.
2) Calculate the voltage at the load section $\left(V_{A A}\right)$ if $Z_{L}$ becomes a short circuit due to a fault in the load; express $V_{A A}$ in the time domain.


## Solution

1) As there is no match at the generator section and at the load section, let us calculate the reflection coefficient at AA:
$\Gamma_{L}=\frac{Z_{L}-Z_{C}}{Z_{L}+Z_{C}}=-0.2$
The reflection coefficient at section BB is:
$\Gamma_{B B}=\Gamma_{L} e^{-2 j \beta l}=0.2$
As a result, the input impedance is:
$\mathrm{Z}_{B B}=\mathrm{Z}_{C} \frac{1+\Gamma_{B B}}{1-\Gamma_{B B}}=112.5 \Omega$
As the line length is a multiple of $\lambda / 4$, the input impedance could have been easily calculated as:
$\mathrm{Z}_{B B}=\frac{Z_{C}^{2}}{Z_{L}}$
The reflection coefficient at the generator section (left side) is:
$\Gamma_{g}=\frac{Z_{B B}-Z_{g}}{Z_{B B}+Z_{g}}=0.3846$
Therefore, the power crossing section BB is:
$P_{B B}=P_{L}=\frac{\left|V_{g}\right|^{2}}{8 \operatorname{Re}\left[Z_{g}\right]}\left(1-\left|\Gamma_{g}\right|^{2}\right)=0.213 \mathrm{~W}$
This is also the power absorbed by the load, as no other element in the circuit beyond section BB can absorb power.
2) If the load becomes a short circuit, there is no need to perform calculations: indeed, as $Z_{L}=0 \Omega \rightarrow$ $\Gamma_{L}=-1$. As a result, whatever the progressive wave reaching the load, it will be totally reflected with a change in the sign. Therefore, the total voltage at the section (progressive+regressive) will always be 0 V (as expected from a short circuit) $\rightarrow V_{A A}(t)=0 \mathrm{~V}$.

## Problem 2

A uniform sinusoidal plane wave propagates in a medium characterized by relative electric permittivity $\varepsilon_{r}=1$, magnetic permeability $\mu_{r}=9$ and conductivity $\sigma=0.1 \mathrm{~S} / \mathrm{m}$. The expression of the electric field is $\left(E_{0}=1 \mathrm{~V} / \mathrm{m}\right)$ :

$$
\vec{E}(z, t)=E_{0} e^{-\alpha z} \cos \left(2 \pi 10^{9} t-\beta z\right) \vec{\mu}_{y} \quad \mathrm{~V} / \mathrm{m}
$$

For such a wave:

1) What is the wave polarization?
2) Calculate the phase velocity of the wave.
3) Calculate the power received by an isotropic antenna located at $\mathrm{P}(0.1 \lambda, 0.1 \lambda, 0.1 \lambda)$, which has efficiency $\eta_{A}=0.9$.


## Solution

1) The wave is linearly polarized (vertical polarization).
2) Let us first check the loss tangent for the wave:
$\tan \delta=\frac{\sigma}{\omega \varepsilon} \approx 1.8$
No approximations can be applied; therefore, the propagation constant is calculated as:
$\gamma=\alpha+j \beta=\sqrt{j \omega \mu(\sigma+j \omega \varepsilon)}=45.7+j 77.71 / \mathrm{m}$
From $\beta$, the phase velocity is calculated as:
$v=\frac{\omega}{\beta}=8.1 \times 10^{7} \mathrm{~m} / \mathrm{s}$
3) The wavelength is given by:
$\lambda=\frac{2 \pi}{\beta}=0.0808 \mathrm{~m}$
Therefore P is in $(0.00808 \mathrm{~m}, 0.00808 \mathrm{~m}, 0.00808 \mathrm{~m})$.
The power received at P by the antenna is:
$P_{R}=S A_{e}=\frac{1}{2} \frac{|\vec{E}(P)|^{2}}{|\eta|} \cos (\Varangle \eta) A_{e}=\frac{1}{2} \frac{\left|E_{0}\right|^{2}}{|\eta|} e^{-2 \alpha z_{P}} \cos (\Varangle \eta) \frac{\lambda^{2}}{4 \pi} D \eta_{A}$
where:
$D=1$ (isotropic antenna with directivity 1 )
$\eta=\sqrt{\frac{j \omega \mu}{(\sigma+j \omega \varepsilon)}}=679+j 399 \Omega$
Therefore:

$$
P_{R}=0.12 \mu \mathrm{~W}
$$

# Electromagnetics and Signal Processing for Spaceborne Applications - SP part 

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## Problem 3

The signal received from a distant source is modeled as

$$
s(t)=A_{-} \cdot \cos \left(2 \pi\left(f_{0}-\frac{\Delta f}{2}\right) t\right)+A_{+} \cdot \cos \left(2 \pi\left(f_{0}+\frac{\Delta f}{2}\right) t\right)
$$

where $f_{0}=1 \mathrm{GHz}$ is the carrier frequency and $\Delta f=1 \mathrm{KHz}$

1. Write the expression of the complex received signal. Tip: remember that the Fourier Transform of the complex signal is the same as the FT of the real-valued signal for positive frequencies, whereas it is identically zero for negative frequencies.
2. Write the expression of the complex envelope (after demodulation by $f_{0}$ )
3. Describe a procedure to measure the two constants $A_{-}$and $A_{+}$based on the complex envelope.
4. For how long a time should you observe the received signal to be able to make a good measurement of $A_{-}$and $A_{+}$?
5. Write a short pseudo-code to implement the procedure at point 3 .

## Solution

The FT of $s(t)$ is

$$
\begin{aligned}
& S(f)=\frac{A_{-}}{2} \delta\left(f-\left(f_{0}-\frac{\Delta f}{2}\right)\right)+\frac{A_{+}}{2} \delta\left(f-\left(f_{0}+\frac{\Delta f}{2}\right)\right)+ \\
& \quad+\frac{A_{-}}{2} \delta\left(f+\left(f_{0}-\frac{\Delta f}{2}\right)\right)+\frac{A_{+}}{2} \delta\left(f+\left(f_{0}+\frac{\Delta f}{2}\right)\right)
\end{aligned}
$$

The lower line represents pulses found at negative frequencies, so it vanishes if only positive frequencies are considered. When returning in the time domain each $\delta$ becomes a complex exponential, thus:

$$
s_{c}(t)=A_{-} \cdot \exp \left(j 2 \pi\left(f_{0}-\frac{\Delta f}{2}\right) t\right)+A_{+} \cdot \exp \left(j 2 \pi\left(f_{0}+\frac{\Delta f}{2}\right) t\right),
$$

The complex envelope is obtained by multiplication by $\exp \left(j 2 \pi f_{0} t\right)$, hence

$$
s_{c e}(t)=A_{-} \cdot \exp \left(-j 2 \pi \frac{\Delta f}{2} t\right)+A_{+} \cdot \exp \left(j 2 \pi \frac{\Delta f}{2} t\right),
$$

The amplitudes can be measured by taking the FT of the complex envelope. If the FT is evaluated over an infinite observation time we get:

$$
s_{c e}(f)=A_{-} \cdot \delta\left(f+\frac{\Delta f}{2}\right)+A_{+} \cdot \delta\left(f-\frac{\Delta f}{2}\right)
$$

So one has to evaluate the area of the two delta.
More realistically, we will get

$$
s_{c e}(f)=A_{-} \cdot T_{o} \operatorname{sinc}\left(\left(f+\frac{\Delta f}{2}\right) T_{o}\right)+A_{+} \cdot T_{o} \operatorname{sinc}\left(\left(f-\frac{\Delta f}{2}\right) T_{o}\right),
$$

So $A_{-}$and $A_{+}$are obtained by taking the peak of the two sinc divided by $T_{o}$
The condition to see two separate peaks is that $T_{o}>\frac{1}{\Delta f}$. Otherwise the two peaks interfere.
Pragmatically, one would like to ensure that $T_{o} \gg \frac{1}{\Delta f}$

## Problem 4



Consider two satellites at a height $\mathrm{H}=1000 \mathrm{Km}$ that transmit a signal at the frequency $f_{0}=1 \mathrm{GHz}$ toward a receiver placed at $x=0$. The positions of the two satellites along the x -axis are $+x_{s}$ and $-x_{s}$, with $x_{s}=500 \mathrm{Km}$.

1. Assuming that the two satellites transmit simultaneously, derive the graph of the field amplitude along the x -axis. Tip: assume small values of $x$, so that you can - as always linearize the expression of the distances w.r.t. the reference position $x=0$.
2. Repeat point 1 assuming that the satellite on the right transmits with a delay of $\Delta t$ seconds w.r.t. the one on the left. Where should you place the receiver to maximize the intensity of the received signal?
3. Imagine now to place a few receivers on the ground (in the neighborhood of $x=0$ ) to measure the angle $\psi$. Discuss the role of the spatial sampling between any two nearby receivers and of the total number of receivers.

## Solution

1) The field in the neighborhood of the receiver is:

$$
E(x)=\frac{1}{R_{1}(x)} \exp \left(-j \frac{2 \pi}{\lambda} R_{1}(x)\right)+\frac{1}{R_{2}(x)} \exp \left(-j \frac{2 \pi}{\lambda} R_{2}(x)\right)
$$

The distances are approximated as:

$$
\begin{aligned}
& R_{1}(x)=\sqrt{H^{2}+\left(x+x_{s}\right)^{2}} \cong R_{0}+\sin \psi \cdot x \\
& R_{2}(x)=\sqrt{H^{2}+\left(x-x_{s}\right)^{2}} \cong R_{0}-\sin \psi \cdot x
\end{aligned}
$$

Where the angle for the two satellites is defined such that $\sin \psi>0$
Hence:
$E(x) \cong \frac{1}{R_{0}} \exp \left(-j \frac{2 \pi}{\lambda} R_{0}\right)\left[\exp \left(-j \frac{2 \pi}{\lambda} \sin \psi \cdot x\right)+\exp \left(+j \frac{2 \pi}{\lambda} \sin \psi \cdot x\right)\right]$
$\cong \frac{2}{R_{0}} \exp \left(-j \frac{2 \pi}{\lambda} R_{0}\right) \cos \left(\frac{2 \pi}{\lambda} \sin \psi \cdot x\right)$
2) If the second transmission is delayed one has:

$$
\begin{aligned}
& E(x) \cong \frac{1}{R_{0}} \exp \left(-j \frac{2 \pi}{\lambda} R_{0}\right)\left[\exp \left(-j \frac{2 \pi}{\lambda} \sin \psi \cdot x\right)+\exp \left(+j \frac{2 \pi}{\lambda} \sin \psi \cdot x\right) \exp \left(-j 2 \pi f_{0} \Delta t\right)\right] \\
& \begin{array}{c}
\cong \frac{1}{R_{0}} \exp \left(-j \frac{2 \pi}{\lambda} R_{0}\right) \exp \left(-j \pi f_{0} \Delta t\right) \\
\cdot \\
{\left[\exp \left(-j \frac{2 \pi}{\lambda} \sin \psi \cdot x\right) \exp \left(j \pi f_{0} \Delta t\right)+\exp \left(+j \frac{2 \pi}{\lambda} \sin \psi \cdot x\right) \exp \left(-j \pi f_{0} \Delta t\right)\right]} \\
\cong \frac{1}{R_{0}} \exp \left(-j \frac{2 \pi}{\lambda} R_{0}\right) \exp \left(-j \pi f_{0} \Delta t\right) \\
\cdot\left[\exp \left(-j \pi\left(\frac{2}{\lambda} \sin \psi \cdot x-f_{0} \Delta t\right)\right)+\exp \left(+j\left(\frac{2}{\lambda} \sin \psi \cdot x-f_{0} \Delta t\right)\right)\right] \\
\cong \frac{1}{R_{0}} \exp \left(-j \frac{2 \pi}{\lambda} R_{0}\right) \exp \left(-j \pi f_{0} \Delta t\right) \\
\cdot\left[\exp \left(-j \pi\left(\frac{2}{\lambda} \sin \psi \cdot x-f_{0} \Delta t\right)\right)+\exp \left(+j\left(\frac{2}{\lambda} \sin \psi \cdot x-f_{0} \Delta t\right)\right)\right]
\end{array} \\
& E(x) \cong \frac{2}{R_{0}} \exp \left(-j \frac{2 \pi}{\lambda} R_{0}\right) \exp \left(-j \pi f_{0} \Delta t\right) \cdot \cos \left(\pi\left(\frac{2}{\lambda} \sin \psi \cdot x-f_{0} \Delta t\right)\right)
\end{aligned}
$$

Field intensity peaks at $x=\frac{\lambda}{2 \sin \psi} f_{0} \Delta t$
From point 1 , the field is proportional to $\cos \left(\frac{2 \pi}{\lambda} \sin \psi \cdot x\right)$. Accordingly, receivers must be placed so as to estimate the frequency of the cosine $\left(f_{x}=\frac{\sin \psi}{\lambda}\right)$ unambiguously, which yields $\Delta x \leq \frac{\lambda}{2}$.
The total number of receivers determines frequency resolution, so with $N$ receivers one has $\Delta f_{x}=$ $\frac{1}{N \Delta x}$, hence $\Delta \psi=\frac{d \psi}{d f_{x}} \Delta f_{x}=\frac{\lambda}{\cos \psi} \frac{1}{N \Delta x}$.

Notice that the analysis yields two peaks at $f_{x}= \pm \frac{\sin \psi}{\lambda}$ (one peak per satellite)

