Radio and Optical Wave Propagation – Prof. L. Luini, July 15th, 2022 – Part 2



Problem 1

The figure below shows a bistatic radar system (carrier frequency $f_1 = 1$ GHz), consisting of two LEO satellites (same orbit, satellite height above the ground H = 500 km, elevation angle $\theta = 45^{\circ}$). The radar extracts information on the atmosphere by measuring the difference between the power received along the direct path and the downlink to the ground station. Making reference to the right, where the electron content (N_e) profile ($h_{\min} = 100$ km, $h_{\max} = 400$ km, $N_m = 5 \times 10^{12}$ e/m³, N homogeneous horizontally) and the tropospheric specific attenuation profile ($\alpha = 0.01e^{-h/50}$, where h is in km and α , horizontally homogeneous, is in dB/km) are shown, and to the left side, where the simplified geometry is reported:

- 1) Calculate the difference of the power received along the two paths.
- 2) Will the difference between the power received along the two paths (compared to point 1) if the frequency changes to $f_2 = 25$ MHz?

Assume: transmit power $P_T = 100$ W; gain of the TX and RX antenna (circular parabolic reflector) G = 45 dB; antenna radiation pattern $f = [\cos(\theta)]^2$, where ϕ is the angle between the specific direction and the antenna axis; perfect pointing for the downlink, on both ends.



Solution

1) The power received along the direct path (free space) is simply given by:

$$P_{R1} = P_T G_T f_T (\lambda/4\pi D)^2 G_R f_R$$

where:

$$D = \frac{2H}{\text{tg}(\theta)}$$

$$G_T = G_R = G$$

$$f_T = f_R = \cos(\theta)$$
Therefore $\rightarrow P_{R1} = 14.2 \,\mu\text{W}$

Regarding the second path, the power density reaching the ground is:

$$S = \frac{P_T}{4\pi L^2} GA_l$$

where $L = H/\sin(\theta)$ and A_l is the tropospheric attenuation (the ionospheric one can be neglected given the carrier frequency in the GHz range). The zenithal tropospheric attenuation can be calculated as:

$$A_{Z} = \int_{0}^{H} \alpha dh = \alpha_{0} \int_{H}^{H_{S}} e^{-\frac{h}{h_{0}}} dh = -\alpha_{0} h_{0} \left[e^{-\frac{h}{h_{0}}} \right]_{0}^{H}$$

As $H >> h_{0} = 50$ km:
 $A_{T} = -\alpha_{0} h_{0} \left[e^{-\frac{h}{h_{0}}} \right]_{0}^{\infty} = \alpha_{0} h_{0} = 0.5$ dB

$$A_Z = -\alpha_0 h_0 \left[e^{-\frac{n}{h_0}} \right]_0 = \alpha_0 h_0 = 0.5 \text{ dB}$$

The slant path attenuation in linear scale is:

$$A_l = 10^{-(A_Z/\sin(\theta))/10} = \alpha_0 h_0 = 0.85 \text{ dB}$$

The power received on the ground is:

$$P_{R2} = SA_{RX} = \frac{P_T}{4\pi L^2} GA_l \frac{\lambda^2}{4\pi} G = 96.9 \,\mu\text{W}$$

The differential power is:

$$\Delta P_R = P_{R2} - P_{R1} = 82.6 \,\mu\text{W}$$

2) Using the second frequency (range of tens of MHz), it is worth checking if the wave can actually cross the ionosphere. For the wave to avoid total reflection due to the ionosphere, the angle θ needs to be higher than θ_{min} , determined as by:

$$\cos(\theta_{min}) = \sqrt{1 - \left(\frac{9\sqrt{N_m}}{f_2}\right)^2} \quad \Rightarrow \quad \theta_{min} = 53.6^\circ$$

As $\theta < \theta_{min}$, the wave will be totally reflected and it will not be received by RX.

Problem 2

A plane EM wave at 30 GHz propagates across a layer of melting hydrometeors (path length d = 1 km, $\theta = 45^{\circ}$ tilt angle), which is characterized by the following propagation constants (see sketch below):

 $\gamma_I = 0.6413 + j628676$ 1/km

 $\gamma_{II} = 0.6413 + j628674.43$ 1/km

The transmitter (TX) employs a vertical linear antenna; as for the RX antenna, see point 2). For this link:

- 1) Determine the wave polarization in front of the receiver (no need to specify the tilt angle for a linear polarization, nor the rotation direction for a circular/elliptical polarization).
- 2) Based on point 1, determine the RX antenna to maximize the received power.
- 3) Based on point 2, calculate the power received by RX.

Assume that:

- the Earth surface is flat; disregard the reflection from the ground and the attenuation due to gases; consider plane wave propagation;
- use the following data: electric filed emitted at TX, $|\vec{E}_{TX}| = 10 \text{ V/m}$; effective area of the RX antenna, $A_{RX} = 1 \text{ m}^2$ (whatever the choice at point 2); assume free space for the calculation of the medium intrinsic impedance.



Solution

1) As is clear from the propagation constants, the hydrometeor slab induces the same attenuation on both I and II components of the wave; on the other hand, the differential phase shift is:

$\Delta\beta = \beta_{II} - \beta_I = -1.57 = -\pi/2 \text{ rad/km}$

The TX antenna emits a vertical polarization, so the amplitude of components I and II are equal and given by $|\vec{E}_{TX}|\cos(45^\circ) = 7.07 \text{ V/m}$. Therefore, in front of RX, the two components I and II will have: 1) same amplitude (attenuated by the slab); 2) a differential phase shift of $\pi/2 \text{ rad/km} \rightarrow$ the polarization will be circular.

2) Given the circular polarization determined at point 1, a circular polarized antenna is the best choice.

3) The received power will be given by:

$$P_{RX} = \frac{1}{2} \frac{\left|\vec{E}_{TX}\right|^2}{\eta_0} e^{-2 \times 0.6413 \times d} A_{RX} = 0.0368 \text{ W}$$

Problem 3

A plane sinusoidal EM wave (f = 9 GHz) propagates from a medium with electric permittivity $\varepsilon_{r1} = 4$ (assume $\mu_r = 1$ for both media) into free space. The expression of the incident electric field is:

$$\vec{E}_i(z, y) = -j\vec{\mu}_x e^{-j\frac{\sqrt{2}}{2}\beta_1 z} e^{j\frac{\sqrt{2}}{2}\beta_1 y}$$
 V/m

1) What is the polarization of the incident field (specify the details of the polarization)?



Solution

1) The wave polarization is linear, specifically a TE component (along -*x*).

2) The incidence angle can be derived, for example, from the *y* component of β : $\beta_y = \beta_1 \sin(\theta) = \beta_1 \sqrt{2}/2 \rightarrow \sin(\theta) = \sqrt{2}/2 \rightarrow \theta = 45^{\circ}$

To determine the transmitted wave, it is first necessary to calculate the refraction angle, which is:

$$\theta_2 = \sin^{-1}\left(\sin\left(\theta\right)\sqrt{\frac{\varepsilon_{r1}}{\varepsilon_{r2}}}\right) = \sin^{-1}(\sqrt{2}) \approx \sin^{-1}(1.4142)$$

This is the sign of an evanescent wave: this wave is totally reflected. The expression of the reflected field will be:

$$\vec{E}_r(z,y) = -j\vec{\mu}_x \Gamma_{TE} e^{j\beta_{1z}z} e^{j\beta_{1y}y} V/m$$

Let us calculate β_{2z} :

$$\beta_{2z} = \beta_2 \cos(\theta_2) = \beta_2 \sqrt{1 - [\sin(\theta_2)]^2} = \beta_0 \sqrt{1 - [\sin(\theta_2)]^2} = \beta_0 \sqrt{1 - \sqrt{2}^2} = \beta_0 \sqrt{-1}$$

= $\pm j\beta_0 = -j\beta_0$

The negative sign is chosen to obtain a physical solution:

$$e^{-j\beta_{2z}z} = e^{-j(-j\beta_0)z} = e^{-\beta_0 z}$$

The reflection coefficient can be calculated as:

$$\eta_1 = \frac{\eta_0}{\cos(\theta)\sqrt{\varepsilon_{r1}}} = 266.6 \,\Omega$$
$$\eta_2 = \frac{\eta_0}{\cos(\theta_2)\sqrt{\varepsilon_{r2}}} = \frac{\eta_0}{-j} = j377 \,\Omega$$

$$\Gamma_{TE} = \frac{\eta_2 - \eta_2}{\eta_2 + \eta_1} = 0.334 + j0.943$$

Therefore, using the expression of the reflected field define above: $\vec{E}_r(A) = \vec{E}_t(z = -1 \text{ m}, y = -1 \text{ m}, x = -1 \text{ m}) = \vec{\mu}_x(0.9756 + j0.2197) \text{ V/m}$

with $\beta_1 = 377.25 \text{ rad/m}$. Obviously $\rightarrow |\vec{E}_r(A)| = 1 \text{ V/m} = |\vec{E}_i|$.

Problem 4

Consider a satellite link, implementing adaptive coding and modulation, which adapts the data rate depending on the link signal to noise ratio (SNR). The link elevation angle is $\theta = 45^{\circ}$ and the link operates at f = 20 GHz. The Complementary Cumulative Distribution Function (CCDF) of the zenithal tropospheric attenuation is given by:

 $P(A_{dB}^Z) = 100e^{-0.545 A_{dB}^Z}$ (A_{dB}^Z in dB and P in %) Determine the yearly time for which 10 Mbit/s can be guaranteed to the user.



$15 \text{ dB} < \text{SNR} \le 20 \text{ dB}$	D = 20 Mbit/s
$10 \text{ dB} < \text{SNR} \le 15 \text{ dB}$	D = 10 Mbit/s
$SNR \le 10 \text{ dB}$	D = 1 Mbit/s

Additional assumptions and data:

- both antennas pointed optimally
- disregard the cosmic background radiation
- power transmitted by each satellite $P_T = 100$ W
- mean radiating temperature $T_{mr} = 290 \text{ K}$
- gain of both antennas G = 35 dB
- satellite altitude H = 600 km
- bandwidth of the receiver: B = 100 MHz
- internal noise temperature of the receiver: $T_R = 300 \text{ K}$

Solution

The signal-to-noise ratio (SNR) is given by

$$SNR = \frac{P_T G_T f_T (\lambda/4\pi L)^2 G_R f_R A}{k[T_R + T_{mr}(1-A)]B}$$

where *k* is the Boltzmann's constant $(1.38 \times 10^{-23} \text{ J/K})$, $f_T = f_R = 1$, $L = H/\sin(\theta)$, $G_R = G_T = G$ (same antenna features). The target data rate is obtained for 10 dB < SNR \leq 15 dB: to calculate the yearly time for which 10 Mbit/s can be guaranteed to the user, the threshold SNR_{min} = 10 dB is used. Therefore, the above equation can be solved for *A* (slant path attenuation in linear scale):

$$A = \frac{SNR_{min}kB(T_R + T_{mr})}{P_T G^2 (\lambda/4\pi L)^2 + SNR_{min}kBT_{mr}} = 0.0041$$

The slant path attenuation in dB is:

 $A_{dB} = -10\log_{10}(A) = 23.9 \text{ dB}$

The zenithal path attenuation in dB is:

 $A_{dB}^{Z} = A_{dB}\sin(\theta) = 16.9 \text{ dB}$

Using such a value in the CCDF of the tropospheric attenuation:

P = 0.01%, which corresponds to approximately 0.89 hours in a year. Therefore, 10 Mbit/s can be guaranteed for 99.99% of the yearly time, i.e. always but 0.89 hours (53 minutes) in a year.