Satellite Communication and Positioning Systems - Prof. L. Luini, September 12 ${ }^{\text {th }}, 2023$

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## Problem 1

Making reference to the figure below, the ionosphere is modelled with the sketched electron density profile, where $N_{\mathrm{m}}=4 \times 10^{12} \mathrm{e} / \mathrm{m}^{3}, h_{\min }=100 \mathrm{~km}$ and $h_{\max }=400 \mathrm{~km}$. The distance between TX and RX is $d=600 \mathrm{~km}$ and the elevation angle $\theta=50^{\circ}$.

1) Calculate the link frequency $f$.
2) Keeping the same operational frequency $f$ found at point 1 ), what happens if the elevation angle is increased to $\theta_{2}=60^{\circ}$ ?

Assume that the virtual reflection height is 1.2 of the height at which the wave is actually reflected.



## Solution

1) The distance $d$ depends on the virtual reflection height as follows:
$d=\frac{2 h_{v}}{\tan \theta}$
Therefore:
$h_{V}=d \frac{\tan \theta}{2}=357.5 \mathrm{~km}$

The real reflection height is:
$h_{R}=\frac{h_{V}}{1.2}=297.9 \mathrm{~km}$
The trend of the electron content with height is:
$N(h)=\frac{N_{m}}{h_{\max }-h_{\min }}\left(h-h_{\min }\right)$ with $h$ in km
The $N$ value at height $h R$ is:
$N\left(h_{R}\right)=2.6 \times 10^{12} \mathrm{e} / \mathrm{m}^{3}$
The link frequency is:

$$
f=\sqrt{\frac{81 N\left(h_{R}\right)}{1-[\cos (\theta)]^{2}}} \approx 19.1 \mathrm{MHz}
$$

2) The maximum frequency guaranteeing reflection for the new elevation angle $\theta_{2}$ is:

$$
f_{\max }=\sqrt{\frac{81 N_{m}}{1-\left[\cos \left(\theta_{2}\right)\right]^{2}}} \approx 20.8 \mathrm{MHz}
$$

As $f<f_{\text {max }}$, the wave is still completely reflected by the ionosphere.

## Problem 2

A radar with zenithal pointing, working at $f=10 \mathrm{GHz}$, illuminates an aircraft flying at altitude $h_{P}=10000 \mathrm{~m}$. As depicted in the figure below, a rain layer (propagation constant in the rain layer $\gamma_{R}=1.7 \times 10^{-4}+j 1.886 \times 10^{3} 1 / \mathrm{m}$; rain height $h_{R}=5000 \mathrm{~m}$ ) affects the radar. Calculate:

1) The time for the pulse to reach back the radar after reflection on the aircraft.
2) The backscatter section of the airplane, knowing that: the radar transmit power is $P_{T}=1 \mathrm{~kW}$; the received power is $P_{R}=0.15 \mathrm{nW}$; the antenna gain is $G=50 \mathrm{~dB}$.


## Solution

1) The wave propagates with different phase velocity in the rain layer and in air. For the former:
$v_{R}=\frac{\omega}{\beta_{R}}=0.33 \times 10^{8} \mathrm{~m} / \mathrm{s}$
while, for the latter, we can assume:
$v_{A}=c=3 \times 10^{8} \mathrm{~m} / \mathrm{s}$
The two-way propagation time is given by:
$\tau=2\left(\int_{0}^{h_{R}} \frac{d s}{v_{R}}+\int_{h_{R}}^{h_{P}} \frac{d s}{v_{A}}\right)=2\left(\frac{h_{R}}{v_{R}}+\frac{h_{P}-h_{R}}{v_{A}}\right)=3.33 \times 10^{-4} \mathrm{~s}$
2) First, the rain attenuation is given by:
$A_{R}=e^{-2 \alpha_{R} h_{R}}=0.1813$
The power density reaching the aircraft is:
$S_{A}=\frac{P_{T}}{4 \pi h_{P}^{2}} G A_{R}=0.0144 \mathrm{~W} / \mathrm{m}^{2}$
The power received back by the radar is:
$P_{R}=\frac{S_{A} \sigma}{4 \pi h_{P}^{2}} A_{R} G \frac{\lambda^{2}}{4 \pi}$
Solving for the backscatter section $\rightarrow \sigma \approx 10 \mathrm{~m}^{2}$.

## Problem 3

Two ground stations operating at $f=15 \mathrm{GHz}$ and $f=30 \mathrm{GHz}$ aim at communicating with a GEO satellite at elevation angle $\theta=45^{\circ}$. For each ground station, and for each refractivity profiles depicted below, state if the elevation angle to be used needs to be higher or lower than $45^{\circ}$ to correctly point at the satellite ( $N_{0}=1000 \mathrm{ppm}, h_{0}=8 \mathrm{~km}$ ).



## Solution

The vertical gradient of the refractivity will induce a change in the propagation direction (ray bending). This effect is frequency independent, therefore the results will be the same for both ground stations.
The curvature radius of the EM wave depends on the refractivity gradient as follows:
$\rho=-\frac{10^{6}}{d N / d h}$
Profile on the left
The refractivity profile is:
$N(h)=-\frac{N_{0}}{h_{0}} h+N_{0} \rightarrow \frac{d N}{d h}=-\frac{N_{0}}{h_{0}}=-125 \mathrm{~km}^{-1}$
Therefore, the curvature radius is:
$\rho_{1}=8000 \mathrm{~km}$
$\rho_{1}$ is positive, so the ray is bent towards the ground: the actual elevation angle will need to be higher than $45^{\circ}$.

## Profile on the right

The refractivity profile is:
$N(h)=N_{0} \quad \rightarrow \frac{d N}{d h}=0 \mathrm{~km}^{-1}$
Therefore, the curvature radius is:
$\rho_{2} \rightarrow \infty$
$\rho_{2}$ indicates that the EM ray will not be curved, so the actual elevation angle will need to be exactly $45^{\circ}$.

## Problem 4

A dual-frequency military receiver, correctly providing the PVT solution, tracks, among the others, a GNSS satellites at distance $r=26248763 \mathrm{~m}$ and at elevation angle $\theta=40^{\circ}$. The wave crosses an ionospheric layer (horizontal homogeneous) with the vertical electron content profile sketched on the right side of the figure below ( $h_{\max }=300 \mathrm{~km}, h_{\min }=80 \mathrm{~km}, N_{\max }=4 \times 10^{12} \mathrm{e} / \mathrm{m}^{3}$ ) and the vertical refractivity profile (horizontal homogeneous, $N_{0}=400, h_{1}=20 \mathrm{~km}, h_{P}=30 \mathrm{~km}$ ) sketched on the left side of the figure below. For this scenario:

1) Knowing that the $\mathrm{L} 2 \mathrm{P}(\mathrm{Y})$-code prompt code correlator value is $C=0.7$, calculate the L 2 range error affecting the receiver for that satellite.


2) The receiver calculates the following DOP matrix:

$$
R=\left[\begin{array}{cccc}
0.23 & -0.04 & -0.22 & -0.14 \\
-0.04 & 0.19 & 0.08 & 0.04 \\
-0.22 & 0.08 & 2.51 & 1.94 \\
-0.14 & 0.04 & 1.94 & 0.97
\end{array}\right]
$$

The receiver is used to land an aircraft. Calculate the positioning error value that is provided for $95.45 \%$ of the time. To this aim, considering that the user-equivalent range error is modelled using the following Probability Density Function ( $d \rho$ expressed in m):

$$
P(d \rho)=\frac{1}{6 \sqrt{2 \pi}} e^{-\frac{d \rho^{2}}{72}}
$$

## Solution

1) The pseudorange is affected by different error sources. The ionospheric delay can be neglected as we deal with a two-frequency receiver. Also the receiver clock bias error can be neglected, as the receiver is correctly providing the PVT solution. As for the zenithal tropospheric delay, it is given by:
$\tau=T-T_{0}=\frac{10^{-6}}{c} \int_{0}^{h_{P}} N d h=\frac{10^{-6}}{c}\left[\frac{N_{0} h_{1}}{2}+\frac{N_{0}\left(h_{P}-h_{1}\right)}{2}\right]=2 \times 10^{-8} \mathrm{~s}$
As a result the tropospheric delay on the pseurorange is:
$d^{T}=c \frac{\tau}{\sin (\theta)}=9.3 \mathrm{~m}$
Considering all the contributions affecting the pseudorange in this case, we obtain:
$\rho=r+d^{T}+d^{P(Y)}$
where $d^{P(Y)}$ is the error due to the correlator
$d^{P(Y)}=c T_{P(Y)}(1-C)=8.8 \mathrm{~m}$
Therefore, the range error is:
$\Delta \rho=d^{T}+d^{P(Y)}=18.1 \mathrm{~m}$
2) To answer the question, let us first calculate PDOP (3D error important for aircrafts) as: $\mathrm{PDOP}=\sqrt{R_{11}+R_{22}+R_{33}}=1.71$
From the Gaussian distribution, the UERE is $\sigma=6 \mathrm{~m}$.
The desired 3D positioning error is given by:
$\sigma_{3 D}=\mathrm{TDOP} 2 \sigma=20.5 \mathrm{~m}$
