

**Satellite Communication and Positioning Systems – Prof. L. Luini,  
August 28<sup>th</sup>, 2024**

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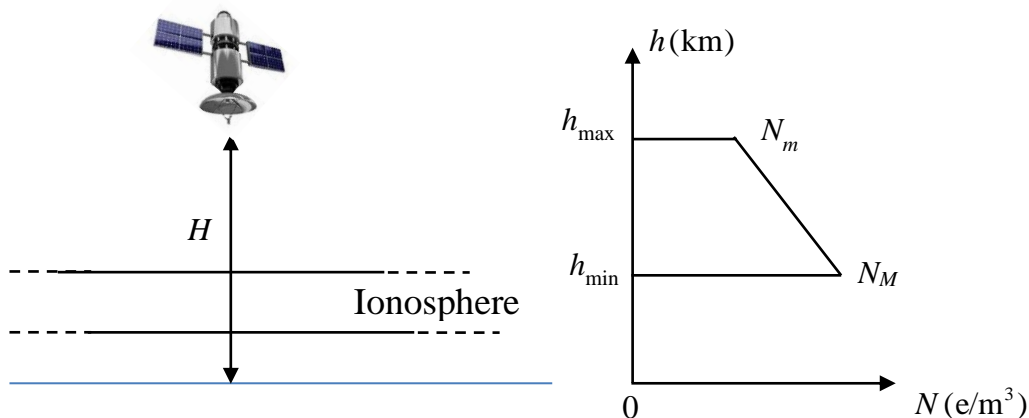
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**Problem 1**

The figure below shows a monostatic radar onboard a LEO satellite, with height above the ground  $H = 700$  km (left side). The radar extracts information on the ionospheric electron content by using concurrent pulses emitted at two carrier frequencies,  $f_1$  and  $f_2$ . Making reference to the electron content profile on the right side ( $N_m = 10^{12}$  e/m<sup>3</sup>,  $N_M = 4 \times 10^{12}$  e/m<sup>3</sup>):

- 1) Determine the maximum frequency  $f_{\max}$  for the associated pulse to be reflected by the ionosphere at  $h_{\max}$ . Set  $f_1 = 0.9f_{\max}$ .
- 2) Determine the minimum frequency  $f_{\min}$  for the associated pulse to be reflected by the ground. Set  $f_2 = 2f_{\min}$ .
- 3) Determine  $h_{\max}$  knowing that the one-way travel time of the pulse at  $f_1$  is  $t_1 = 1$  ms.
- 4) Determine  $h_{\min}$  knowing also that the one-way travel time of the pulse at  $f_2$  is  $t_2 = 2.411072$  ms.

Assumption: neglect tropospheric effects.



**Solution**

1) To determine the carrier frequency  $f_1$  for the pulse to be reflected at  $h_{\max}$ , the following expression can be used:

$$\cos(90) = \sqrt{1 - \left(\frac{9\sqrt{N_m}}{f_{\max}}\right)^2} \Rightarrow f_{\max} = 9\sqrt{N_m} = 9 \text{ MHz} \Rightarrow f_1 = 0.9f_{\max} = 8.1 \text{ MHz}$$

2) To determine the carrier frequency  $f_2$  for the pulse to be reflected at the ground, i.e. crossing the bottom part of the ionosphere at the highest electron content value (at  $h_{\min}$ ), the following expression can be used again:

$$\cos(90) = \sqrt{1 - \left(\frac{9\sqrt{N_M}}{f_{\min}}\right)^2} \Rightarrow f_{\min} = 9\sqrt{N_M} = 18 \text{ MHz} \Rightarrow f_2 = 2f_{\min} = 36 \text{ MHz}$$

3) The pulse at  $f_1$  travels through free space, so its single-way travel time is simply:

$$t_1 = \frac{H - h_{\max}}{c} = 1 \text{ ms} \Rightarrow h_{\max} = 400 \text{ km}$$

4) The pulse at  $f_2$  travels partially through free space, and partially through the ionosphere. Its single-way travel time is therefore:

$$t_2 = \frac{H}{c} + \frac{40.3}{cf_2^2} TEC = 2.411072 \text{ ms}$$

The total electron content is given by:

$$TEC = (h_{\max} - h_{\min})N_m + \frac{(h_{\max} - h_{\min})(N_M - N_m)}{2}$$

Using both equations and solving for the only unknown  $h_{\min}$ :

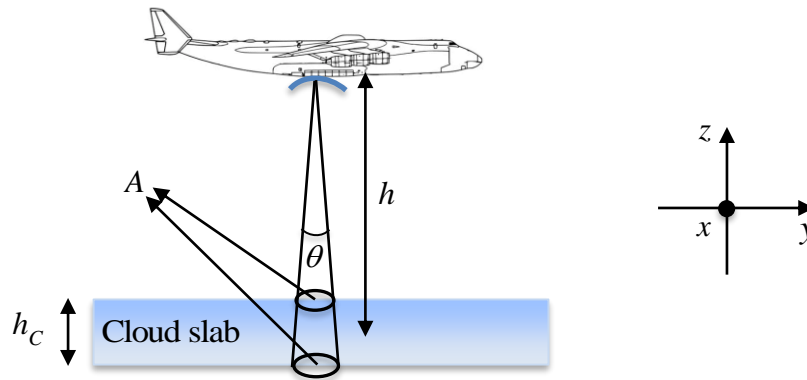
$$h_{\min} = 100 \text{ km}$$

## Problem 2

Making reference to the figure below, a pulsed radar onboard an airplane, operating with carrier frequency  $f = 80$  GHz and pointed zenithally, is used to measure the cloud liquid water content. The wave has RHCP. The beam illuminates a volume  $V$  filled with rain at distance  $h = 5$  km. The area of the volume is  $A = 200$  m<sup>2</sup> and its height is  $h_C = 500$  m. The cloud droplets have density  $N = 100000$  drops/m<sup>3</sup> and they all have the same backscatter section, i.e.  $\sigma = 2$  μm<sup>2</sup>.

- 1) Calculate the power received by the radar  $P_R$ , when the transmit power is  $P_T = 500$  W.
- 2) What is the polarization of the wave received by the radar?

Consider the following: radar antenna gain  $G = 50$  dB; assume negligible cloud attenuation.



## Solution

1) First, let us calculate the power density reaching the rain volume:

$$S = \frac{P_T}{4\pi h^2} G f = 0.1592 \text{ W/m}^2$$

where  $G = 10^5$ ,  $f = 1$  (radar pointing to the volume).

The power reirradiated by a single rain drop is (with gain = 1 according to the definition of backscatter section), is:

$$P_d = S\sigma$$

Considering all the drops in the volume and under the assumption of Wide Sense Stationary Uncorrelated Scatterers (based on which we can sum the power reirradiated by the single drops), we obtain:

$$P_t = NAh_C S\sigma = 0.0032 \text{ W}$$

Finally, the power received by the radar is:

$$P_R = \frac{P_t}{4\pi h^2} A_E = \frac{P_t}{4\pi h^2} G \frac{\lambda^2}{4\pi} = 1.133 \text{ pW}$$

2) The droplets are spherical, so they do not induce a change in the wave polarization. However, the reflection of the wave (backscatter) changes the wave polarization from RH to LH.

### **Problem 3**

Considering the GPS service:

- 1) Which is the most detrimental effect limiting the position accuracy in common receivers? Justify your answer.
- 2) Is the positioning more accurate and robust during the satellite acquisition phase or the satellite tracking phase (considering the same number of satellites used for the PVT solution in both cases)? Why?

### **Solution**

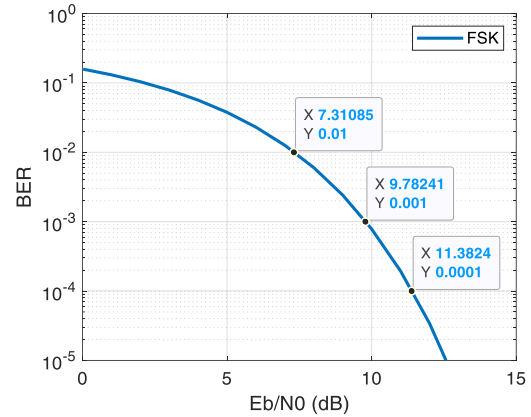
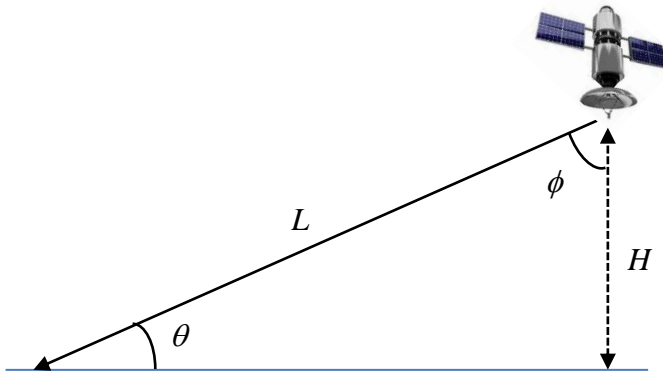
1) Common receivers use only the C/A code, i.e. the information broadcast using only one carrier frequency. Single-frequency receivers are most affected by the ionosphere: the strong delay induced by the ionosphere cannot be completely removed and, in addition, it varies significantly in space and time. Also, in equatorial/tropical regions, ionospheric scintillations causes the receiver loss of lock on the carrier.

2) The PVT solution is more accurate and robust in the satellite tracking phase, mainly due to the integration used for the code correlation: in the acquisition phase, i.e. before bit synchronization, the integration time is typically much shorter than the one used during the tracking phase.

## Problem 4

Consider a link from a LEO satellite to a ground station, operating at  $f = 26$  GHz. For this system, determine the link availability, considering that the link elevation angle is  $\theta = 30^\circ$  and that the BER needs to be lower than  $10^{-4}$  using the FSK modulation (see graph on the right). The CCDF of the zenithal tropospheric attenuation is given by:

$$P(A_T^{dB}) = 100e^{-1.1511A_T^{dB}} \quad (A_T \text{ in dB and } P \text{ in } \%)$$



Additional assumptions and data:

- use the simplified geometry depicted above (left side)
- the specific attenuation of the troposphere is homogeneous vertically and horizontally
- ground station tracking the satellite optimally
- power transmitted by the satellite  $P_T = 160$  W
- disregard the cosmic background contribution
- no additional losses at the transmitter and at the receiver
- LEO satellite pointing always to the centre of the Earth
- radiation patten of the LEO satellite antenna (circular symmetry):  $f_T = [\cos(\phi)]^2$
- mean radiating temperature  $T_{mr} = 288$  K
- gain of the antenna on board the satellite  $G_S = 13$  dB
- gain of the antenna at the ground station  $G_G = 40$  dB
- altitude of the LEO satellite:  $H = 700$  km
- bandwidth of the receiver:  $B = 2$  MHz
- internal noise temperature of the receiver:  $T_R = 300$  K

## Solution

For the BER to be lower than  $10^{-4}$ , the target signal-to-noise ratio (SNR) is  $11.38$  dB =  $13.74$ . The SNR is given by:

$$SNR = \frac{P_T G_S f_T (\lambda/4\pi L)^2 G_G f_R A}{k[T_R + T_{mr}(1 - A)]B}$$

where  $k$  is the Boltzmann's constant ( $1.38 \times 10^{-23}$  J/K),  $f_T = [\cos(90^\circ - \theta)]^2 = 0.25$ ,  $f_R = 1$ ,  $A$  is the slant path tropospheric attenuation (in linear scale), and  $L = H/\sin(\theta) = 1400$  km. Setting the SNR =  $11.38$  dB =  $13.74$ , and solving for  $A$ :

$$A = 0.063 \rightarrow A^{dB} = 12 \text{ dB}$$

The attenuation scaled to the zenith is:

$$A_T^{dB} = A^{dB} \sin(\theta) = 6 \text{ dB.}$$

Using this value in the CCDF expression, we obtain  $P(A_T^{dB}) = 0.1\%$ , which is the link outage probability. The link availability is therefore 99.9%.