

**Telecommunication Systems**  
**January 24<sup>th</sup>, 2019**

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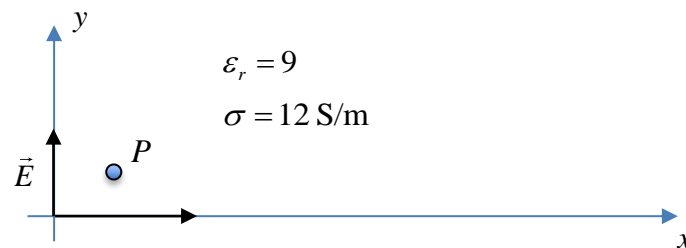
**Problem 1**

A uniform sinusoidal plane wave with frequency  $f = 800$  MHz propagates in a medium characterized by relative electric permittivity  $\epsilon_r = 9$ , magnetic permeability  $\mu_r = 1$  and conductivity  $\sigma = 12$  S/m. The expression of the electric field is ( $E_0 = 10$  V/m):

$$\vec{E} = E_0 e^{-\alpha x} e^{-j\beta x} \vec{\mu}_y \text{ V/m}$$

For such a wave, calculate:

1. the attenuation constant  $\alpha$  and the phase constant  $\beta$
2. the coordinates, in meters, of point  $P(\lambda, \lambda)$ , where  $\lambda$  is the wavelength
3. the power received by an antenna located at P with equivalent reception area  $A_e = 1 \text{ m}^2$



**Solution**

1) Let us first check the loss tangent for the wave:

$$\tan \delta = \frac{\sigma}{\omega \epsilon} \approx 30$$

The medium can be considered as a good conductor, which is very dissipative. As a consequence, the following approximations can be used to calculate the propagation constant ( $\mu = \mu_0$ ):

$$\gamma = \alpha + j\beta = \sqrt{\frac{\omega \mu \sigma}{2}} + j \sqrt{\frac{\omega \mu \sigma}{2}} = 194.68 + j194.68 \text{ 1/m}$$

2) The wavelength is:

$$\lambda = \frac{2\pi}{\beta} = 0.0323 \text{ m}$$

Therefore P is in (0.0323 m, 0.0323 m).

3) The power received at P by the antenna is:

$$P = SA_e = \frac{1}{2} \frac{|\vec{E}(P)|^2}{|\eta|} \cos(\angle \eta) A_e = \frac{1}{2} \frac{|E_0|^2}{|\eta|} e^{-2\alpha x_p} \cos(\angle \eta) A_e \text{ W}$$

where  $x_p = 0.0323 \text{ m}$  and (considering the good conductor approximations):

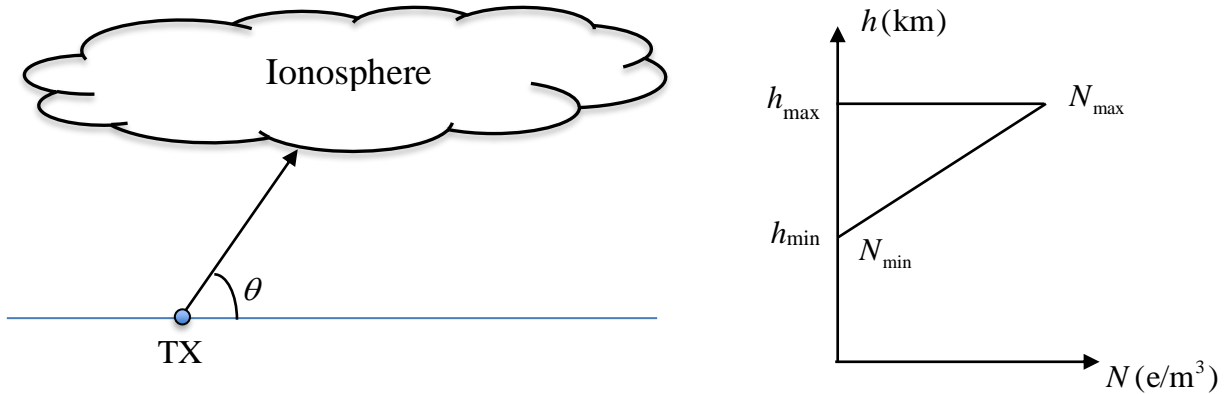
$$\eta = \sqrt{\frac{\mu\omega}{2\sigma}}(1+j) = 16.22(1+j) \ \Omega$$

Therefore:

$$P = 5.37 \ \mu\text{W}$$

## Problem 2

Making reference to the figure below, the ionosphere is modelled with the sketched electron density profile, where  $N_{\max} = 4 \times 10^{12} \text{ e/m}^3$ ,  $N_{\min} = 1 \times 10^{12} \text{ e/m}^3$ ,  $h_{\min} = 100 \text{ km}$  and  $h_{\max} = 400 \text{ km}$ . Determine the minimum operational frequency  $f_{GEO}$  to reach a geostationary satellite, seen at  $\theta = 50^\circ$  elevation from the ground station in TX.



## Solution

1) The minimum frequency necessary to reach the geostationary satellite  $f_{GEO}$ , for a given elevation angle  $\theta$ , is obtained by inverting:

$$\cos \theta = \sqrt{1 - \left( \frac{f_C}{f_{GEO}} \right)^2} = \sqrt{1 - \left( \frac{9\sqrt{N_{\max}}}{f_{GEO}} \right)^2}$$

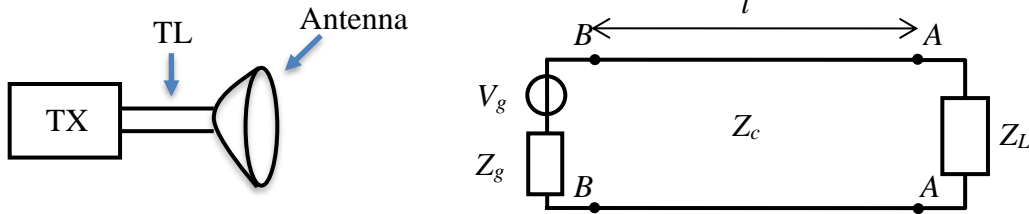
which yields (assuming  $\theta = 50^\circ$ ):

$$f_C = \sqrt{\frac{81N_{\max}}{1 - [\cos(\theta_{GEO})]^2}} \approx 23.5 \text{ MHz}$$

For any frequency higher than  $f_C$ , TX will reach the GEO satellite.

### Problem 3

A transmitter TX with voltage  $V_g = 100$  V and internal impedance  $Z_g = 50 \Omega$  is connected to a transmitting antenna acting as a load ( $Z_L$ ) by a lossless transmission line TL with characteristic impedance  $Z_C = 150 \Omega$ . The line length is  $l = 6$  m and the frequency is  $f = 300$  MHz. Calculate the power radiated by the antenna (i.e. absorbed by the load),  $P_L$ , if the antenna radiation resistance is  $Z_L = 50 \Omega$ .



### Solution

The wavelength is:

$$\lambda = \lambda_0 = c/f = 1 \text{ m}$$

There is a discontinuity at the load section, but the line length  $l$  is a multiple of the wavelength. Therefore, the input impedance at section BB is  $Z_{BB} = 50 \Omega$ . In fact:

$$\Gamma_A = \frac{Z_L - Z_C}{Z_L + Z_C} = -0.5$$

The reflection coefficient at section BB is:

$$\Gamma_B = \Gamma_A e^{-j2\beta l} = \Gamma_A e^{-j2\left(\frac{2\pi}{\lambda}\right)6\lambda} = \Gamma_A e^{-j24\pi} = -0.5$$

Therefore, the input impedance is:

$$Z_B = Z_C \frac{1 + \Gamma_B}{1 - \Gamma_B} = 50 \Omega$$

The reflection coefficient at the generator section is:

$$\Gamma_g = \frac{Z_B - Z_g}{Z_B + Z_g} = 0$$

Therefore, the power crossing section BB, i.e. reaching the load is:

$$P_L = P_{AV} (1 - |\Gamma_g|^2) = \frac{|V_g|^2}{8 \text{Re}[Z_g]} = 25 \text{ W}$$

All the power made available by the transmitter is radiated by the antenna.

#### Problem 4

Consider the downlink from a GEO satellite to a ground station: the elevation angle is  $\theta = 40^\circ$  and link operating frequency is  $f = 30$  GHz. Calculate the signal-to-noise ratio (SNR) using the following data:

- both the ground and satellite antenna have directivity function that can be modelled as:

$$f(\theta) = [\cos(\theta)]^5$$

where  $\theta$  is the angle defining any deviation from the antenna axis (the antenna is parabolic with circular symmetry)

- the equivalent area of the both antennas is  $A_e = 1 \text{ m}^2$
- the ground antenna is optimally pointed to the satellite, while the satellite is mispointed by an angle  $\theta = 20^\circ$
- the power transmitted by the satellite is  $P_T = 100 \text{ W}$
- the distance between the ground station and the satellite is  $H = 38000 \text{ km}$
- the receiver LNA equivalent noise temperature is  $T_{LNA} = 150 \text{ K}$
- the antenna equivalent noise temperature  $T_A = 85 \text{ K}$
- on-board losses  $L_{SAT} = 0.3 \text{ dB}$
- receiver waveguide losses  $L_R = 0.8 \text{ dB}$  (waveguide temperature  $T_{WG} = 40^\circ$ )
- system bandwidth  $B = 500 \text{ MHz}$
- cloud and gases attenuation  $A_{GC} = 1.5 \text{ dB}$

What happens to the SNR if rain starts to fall? Which terms of the SNR equation will be affected by the additional presence of rain?

#### Solution

1) The wavelength is  $\lambda = c/f = 0.01 \text{ m}$ . The gain of the two antennas is:

$$G_T = G_R = \frac{4\pi}{\lambda^2} A_e \approx 125664 = 51 \text{ dB}$$

The on-board and ground losses are:

$$L_{SAT} = 0.3 \text{ dB} = 0.93$$

$$L_R = 0.8 \text{ dB} = 0.83$$

The atmospheric attenuation is:

$$A_{GC} = 1.5 \text{ dB} = 0.71$$

The received power is:

$$P_R = P_T G_T f_T L_{SAT} \left( \frac{\lambda}{4\pi H} \right)^2 G_R f_R L_R A_{GC}$$

where  $f_T(20^\circ) = [\cos(20^\circ)]^5 = 0.73$  and  $f_R = 1$  (the ground antenna is optimally pointed to the satellite). As a result:

$$P_R \approx 2.78 \times 10^{-10} \text{ W}$$

The noise power depends on the total system equivalent noise temperature:

$$T_{\text{sys}} \approx T_A + T_{LR} + T_{LNA}$$

The noise introduced by the waveguide  $T_{LR}$  is given by:

$$T_{LR} = T_{WG} (1-L_R) = 52.7 \text{ K}$$

$$\text{Thus } T_{sys} \approx 287.7 \text{ K}$$

The SNR is:

$$SNR = \frac{P_R}{P_N} = \frac{P_R}{kT_{sys}B} = 138.9 = 21.4 \text{ dB}$$

where  $k$  is the Boltzmann's constant ( $1.38 \times 10^{-23}$  J/K).

The presence of rain will increase the atmospheric attenuation, thus reducing the received power, and, at the same time, it will also increase the noise power through the increase in  $T_A$ . Both effects will concur to reducing the SNR.

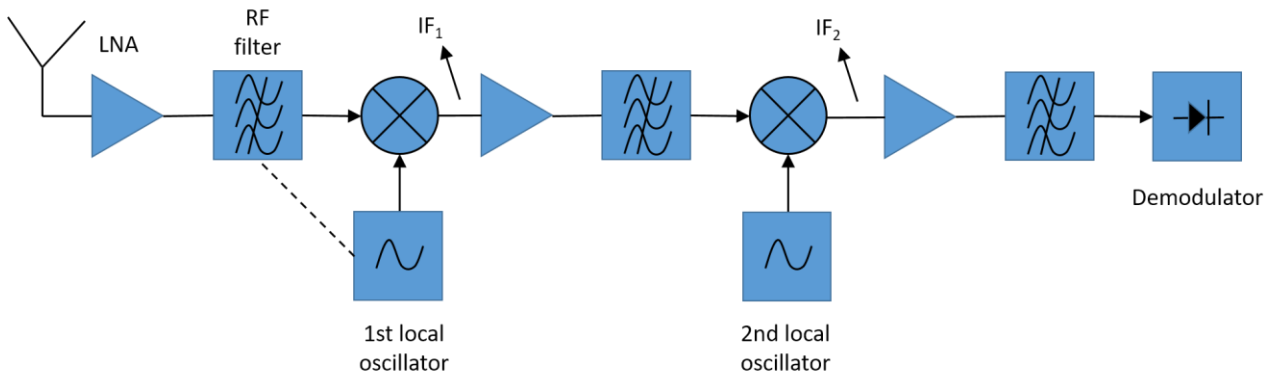
### Problem 5

A superheterodyne receiver (double conversion) is used in a satellite system operating at 10 GHz with 5 MHz channel bandwidth.

1. Show the block diagram of the receiver and briefly comment the general characteristics of each subsystem.
2. Propose a frequency plan ( $f_{IF1}$ ,  $f_{IF2}$ ,  $f_{osc1}$ ,  $f_{osc2}$ ) and justify the choice.
3. Evaluate the total gain of the receiver chain assuming that the input voltage at the RF section is 25  $\mu\text{V}$  and the demodulator requires 0.5 V as input.

### Solution

1) The typical block diagram is composed by an RF stage (Low Noise Amplified plus filter to reject the image frequency), a first downconverter (mixer with local oscillator plus amplifier and filter) producing an intermediate frequency high enough to facilitate the rejection of the image frequency using the RF filter, and a second downconverter (mixer with very stable local oscillator plus amplifier and filter) tuned to obtain a lower intermediate frequency but high enough to facilitate the post processing of the signal (sampling).



2) A good choice for the mixer frequencies is:

$$f_{LO1} = 9.9 \text{ GHz}$$

$$f_{LO2} = 90 \text{ MHz}$$

This yields:

$$f_{IF1} = 100 \text{ MHz}$$

$$f_{IF2} = 10 \text{ MHz}$$

3) The gain is given by:

$$G = 20 \log_{10} \left( \frac{0.5}{25 \cdot 10^{-6}} \right) = 86 \text{ dB}$$

We need to add the loss due to the filters (1 dB) and to the mixers (12 dB). Therefore the total gain is 99 dB.