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## Problem 1

Making reference to the figure below, the transmitter TX, working at $f=18 \mathrm{MHz}$, reaches the user RX, at a distance $d$, by exploiting the ionophere. TX transmits with elevation angle $\theta=60^{\circ}$. The ionosphere can be modelled with the symmetric electron density profile sketched in the figure (right side), where $h_{\max }=450 \mathrm{~km}, h_{\min }=100 \mathrm{~km}$ and $N_{\max }=3 \times 10^{12} \mathrm{e} / \mathrm{m}^{3}$.

1) Calculate the distance $d$.
2) Calculate the distance $d$ when $\theta=70^{\circ}$.

Assume that the virtual reflection height $h_{V}$ is 1.2 of the height at which the wave is actually reflected.



## Solution:

1) Considering the figure below, given the distance between the $T X$ and $R X$ and the elevation angle:
$d=\frac{2 h_{V}}{\tan \theta}$
First we need to find where the reflection occurs, which can be obtained by inverting the following formula:
$\cos \theta=\sqrt{1-\left(\frac{f_{P}}{f}\right)^{2}}=\sqrt{1-\left(\frac{9 \sqrt{N}}{f}\right)^{2}}$
This yields:
$N=\frac{\left[1-(\cos \theta)^{2}\right] f^{2}}{81} \approx 3 \times 10^{12} \mathrm{e} / \mathrm{m}^{3}$
As $N=N_{\max }$, the reflection occurs at the height of the profile peak, i.e.:
$h_{R}=h_{\text {min }}+\left(h_{\text {max }}-h_{\text {min }}\right) / 2=275 \mathrm{~km}$
The virtual reflection height is therefore $h_{V}=1.2 h_{R}=330 \mathrm{~km}$.


Therefore:
$d \approx 381 \mathrm{~km}$
2) When the elevation angle increases beyond $60^{\circ}$, RX cannot be reached because the wave crosses the ionosphere.

## Problem 2

A plane sinusoidal wave at $f=3 \mathrm{GHz}$ propagates in the vacuum and impinges orthogonally on a medium characterized by $\varepsilon_{r 2}=4, \mu_{r 2}=1$ and $\sigma_{2}=0.6676 \mathrm{~S} / \mathrm{m}$. The electric field in $(z=0 \mathrm{~m})$ is $\vec{E}_{0}=-5 e^{j 2 \pi} \vec{\mu}_{x} \mathrm{~V} / \mathrm{m}$. Write the full expression of the electric field in the second medium and calculate the power received the parabolic antenna in $\mathrm{A}(z=0.2 \mathrm{~m}, y=0.2 \mathrm{~m}, x=0.2 \mathrm{~m})$ that has the following features: diameter $d=1.6 \mathrm{~m}$, efficiency $\eta=0.5$, same polarization as the wave polarization.


## Solution:

The problem concerns a TEM plane wave polarized along $-x$, i.e.:
$\vec{E}_{i}=-E_{0} \vec{\mu}_{x} e^{-j \beta_{1} z}=-5 \vec{\mu}_{x} e^{-j \beta_{1 z}} \mathrm{~V} / \mathrm{m}$


The intrinsic impedances of the two media (no approximations are possible for the lossy medium as the loss tangent is equal to 1 ) are:
$\eta_{1}=\eta_{0}=377 \Omega$
$\eta_{2}=\sqrt{\frac{j \omega \mu_{0} \mu_{r 2}}{\sigma+j \omega \varepsilon_{0} \varepsilon_{r 2}}}=146.3+j 60.6 \Omega$
The reflection coefficient is therefore:
$\Gamma=\frac{\eta_{2}-\eta_{1}}{\eta_{2}+\eta_{1}}=-0.4271+j 0.1647$
The electric field at the boundary between the two media is given by:
$\vec{E}_{t}(0)=\vec{E}_{i}(1+\Gamma)=-5 \vec{\mu}_{x}(0.5783+j 0.1647)=(-2.8916-j 0.8233) \vec{\mu}_{x} \mathrm{~V} / \mathrm{m}$
The full expression of the electric field in the second medium is:
$\vec{E}_{t}(z)=\vec{E}_{t}(0) e^{-\gamma_{2} z}=\vec{E}_{t}(0) e^{-\left(\alpha_{2}+j \beta_{2}\right) z} \mathrm{~V} / \mathrm{m}$
Therefore, for $z=0.2 \mathrm{~m}$ (the other coordinates are useless as it is a plane wave):
$\vec{E}_{t}(z=0.2 \mathrm{~m})=\vec{E}_{t}(0) e^{-\gamma_{2} 0.2}=1.95 \times 10^{-5}+j 2.56 \times 10^{-5} \mathrm{~V} / \mathrm{m}$
The propagation constant in the second medium is:
$\gamma_{2}=\sqrt{j \omega \mu_{2}\left(\sigma+j \omega \varepsilon_{2}\right)}=57.2+j 138.2 \mathrm{~m}^{-1}$
The equivalent area of the antenna is:
$A_{E}=\eta\left(\frac{d}{2}\right)^{2} \pi=1 \mathrm{~m}^{2}$
The power received by the antenna in A is:
$P=S_{t} A_{E}=\frac{1}{2}\left|\vec{E}_{t}(z=0.2 \mathrm{~m})\right|^{2} \operatorname{Re}\left\{\frac{1}{\eta_{2}}\right\} A_{E}=\frac{1}{2} \frac{\left|\vec{E}_{t}(z=0.2 \mathrm{~m})\right|^{2}}{\left|\eta_{2}\right|} \cos \left(\angle \eta_{2}\right) A_{E} \approx 3 \mathrm{pW}$

## Problem 3

Consider the typical receiver sketched in the figure below. The antenna is modeled as a voltage generator $V_{g}=100 \mathrm{~V}$ (with internal impedance $Z_{g}=50 \Omega$ ), which is connected to the receiver RX through a lossy waveguide (WG) with characteristic impedance $Z_{C}=50 \Omega$ and attenuation constant $\alpha=50 \mathrm{~dB} / \mathrm{km}$. The input impedance of the receiver is $Z_{L}=75 \Omega$, and the frequency is $f=9 \mathrm{GHz}$.

1) Determine the maximum length $l$ to guarantee that the power absorbed by the load $Z_{L}$ is at least $P_{\text {min }}=20 \mathrm{~W}$.
2) Considering that the antenna noise temperature is $T_{A}=100 \mathrm{~K}$ and that $Z_{L}$ is a LNA with equivalent noise temperature $T_{R}=300 \mathrm{~K}$, calculate the total noise power of the receiver; to this aim, assume that the WG physical temperature is $t_{W G}=20^{\circ} \mathrm{C}$ and that the receiver bandwidth is $B=5 \mathrm{MHz}$.


## Solution

1) Given the value of $Z_{L}, Z_{C}$ and $Z_{g}$, the power absorbed by the load is:

$$
P_{L}=P_{A V} e^{-2 \alpha l}\left(1-\left|\Gamma_{L}\right|^{2}\right)
$$

where:
$P_{A V}=\frac{\left|V_{g}\right|^{2}}{8 \operatorname{Re}\left[Z_{g}\right]}=25 \mathrm{~W}$
and
$\Gamma_{L}=\frac{Z_{L}-Z_{C}}{Z_{L}+Z_{C}}=0.2$
Also, $\alpha=5.8 \times 10^{-3} \mathrm{~Np} / \mathrm{m}$
By imposing $P_{L}=P_{\text {min }}$ and solving for $l$ :

$$
\begin{aligned}
& P_{L}=P_{A V} e^{-2 \alpha l}\left(1-\left|\Gamma_{L}\right|^{2}\right)=P_{\min } \\
& l=\frac{\ln \left[P_{\min } / P_{A V}\left(1-\left|\Gamma_{L}\right|^{2}\right)\right]}{-2 \alpha} \approx 15.84 \mathrm{~m}
\end{aligned}
$$

2) The attenuation introduced by the waveguide is:
$A=\frac{P_{L}}{P_{A V}}=0.8$

Therefore, the equivalent noise temperature of the waveguide is:
$T_{W G}=t_{W G}(1-A)=58.6 \mathrm{~K}$
Finally, the noise power is:

$$
P_{N}=k\left(T_{A}+T_{R}+T_{W G}\right) B=3.2 \times 10^{-14} \mathrm{~W}
$$

## Problem 4

Consider a zenithal downlink (elevation angle $\theta=90^{\circ}$ ) from a satellite to a ground station, operating at $f=19 \mathrm{GHz}$, in which the signal goes through a uniform ice cloud (thickness $h=4 \mathrm{~km}$ ) consisting of equioriented ice needles. The propagation constants for the ice cloud are $\gamma_{H}=0.02+\mathrm{j} 1194 \mathrm{~km}^{-1}$ and $\gamma_{V}=0.02+\mathrm{j} 1195.57 \mathrm{~km}^{-1}$ ( V and H are associated to the vertical and horizontal wave polarization, respectively) and they are uniform throughout the whole cloud. Knowing that the satellite transmits a left-end circular polarization (LHCP):

1) Determine the polarization in front of the receiver.
2) Calculate the signal-to-noise ratio of the ground receiver.

Additional data:

- antennas are optimally pointed
- the antenna on the ground receives LHCP waves
- cloud temperature $T_{\text {ice }}=-2{ }^{\circ} \mathrm{C}$
- gain of the antennas (on board the satellite and on the ground): $G_{T}=G_{R}=20 \mathrm{~dB}$
- power transmitted by the satellite: $P_{T}=50 \mathrm{~W}$
- altitude of the satellite: $H=500 \mathrm{~km}$
- bandwidth of the ground receiver: $B=2.5 \mathrm{MHz}$
- internal noise temperature of the receiver: $T_{R}=300 \mathrm{~K}$
- receiver waveguide loss $L_{W G}^{d B}=1 \mathrm{~dB}$
- receiver waveguide physical temperature $t_{W G}=20^{\circ} \mathrm{C}$


## Solution:

1) A LHCP wave consists of two orthogonal linear components with the same amplitude and a differential phase shift of $90^{\circ}$. Looking at the propagation constants, the ice cloud causes the same amount of attenuation on both components, as expected due to the spherical shape of the droplets. In fact, the real part of such constants is:
$\alpha=0.02 \mathrm{~Np} / \mathrm{km}=0.1736 \mathrm{~dB} / \mathrm{km}$
which means that at the receiver the two components will still have the same amplitude.
The cloud also causes a total differential phase shift of:
$\Delta \beta=\beta_{H}-\beta_{V}=\frac{\pi}{2} \mathrm{rad} / \mathrm{km}$
The total phase shift added by the ice cloud is:
$\Delta \phi=\Delta \beta h=2 \pi \mathrm{rad}$
As a result the total differential phase shift between the two components will be:
$\Delta \phi_{\text {TOT }}=\Delta \phi+\frac{\pi}{2}=\frac{\pi}{2}$
Therefore at the receiver the two linear components will still produce a LHCP wave.
2) The signal-to-noise ratio (SNR) is given by:
$S N R=\frac{P_{R}}{P_{N}}=\frac{P_{T} G_{T} f_{T}(\lambda / 4 \pi H)^{2} G_{R} f_{R} A_{C} L_{W G}}{k\left(T_{R}+T_{A}+T_{W G}\right) B}$
where $k$ is the Boltzmann's constant $\left(1.38 \times 10^{-23} \mathrm{~J} / \mathrm{K}\right), T_{A}$ is the antenna noise temperature, $T_{W G}$ is the noise temperature added by the waveguide, $f_{R}=f_{T}=1$ (antenna optimally pointed), $A_{C}$ is the attenuation induced by the ice cloud and $L_{W G}$ is the waveguide loss; finally $\lambda=c / f=0.0158 \mathrm{~m}$.
Calculating the terms in the equation above

- $A_{C}^{d B}=\alpha h=0.7 \rightarrow A_{C}=0.8521$
- $L_{W G}=0.7943$
- $T_{A}=T_{\text {ice }}\left(1-A_{C}\right)=40.1 \mathrm{~K}$
- $T_{W G}=t_{W G}\left(1-L_{W G}\right)=60.2 \mathrm{~K}$
we obtain:
$\mathrm{SNR}=154.7=21.9 \mathrm{~dB}$

